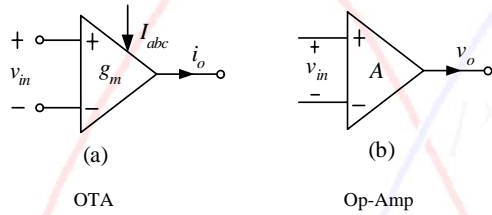


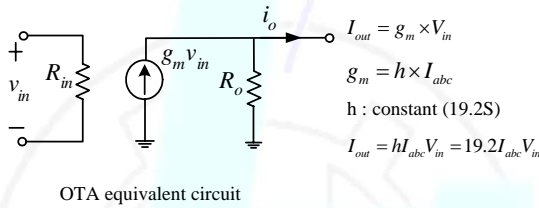
BACKGROUND OPERATIONAL TRANSCONDUCTANCE AMPLIFIER



g_m : amplifier gain
 i_o : Output current
 I_{abc} : amplifier bias current, key parameter to vary gain

A : amplifier gain
 v_o : Output voltage
No reconfigurable gain

MOTIVATION PRACTICAL OTA PERFORMANCE



- Performance characteristics:
 Describe the performance of actual OTAs
- Input/output impedance: ideal $R_{in}/R_o = \infty$
 - Input offset voltage V_{offset} : ideal $V_{offset} = 0$
 - Input offset current I_{offset} : ideal $I_{offset} = 0$
 - Power consumption: heating can not go beyond a threshold
 - Transconductance linearity: decides the reconfigurable range of the generator inertial constant
 - Working frequency: related to the emulation speed

OBJECTIVE

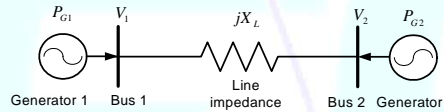
Identify, qualify and quantify the accuracy of OTA-based applications a given power system emulator,
 Investigate the parameter settings for the reconfigurable OTAs,
 Provide feasible OTA applications for power system emulation.

OVERVIEW

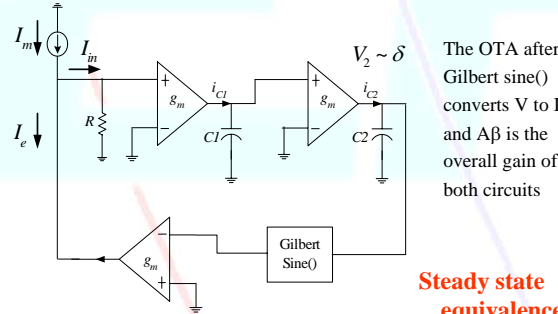
The work identifies, qualifies and then quantifies the features of Operational Transconductance Amplifiers (OTAs) that will make them feasible for power system emulation. The unique feature of OTA is its gain is reconfigurable through an external current source, which makes the OTA-based circuits programmable so that the emulator for power system can do multi-scenario analysis. However, the reconfigurable gain also makes the OTA-based circuit more complicated. In this work, the emulator for one-generator infinite-bus power system is used as an example, and the accuracy and sensitivity of OTA-based circuits in the emulator are analyzed so that they are feasible for power system emulation.

CLASSICAL POWER SYSTEM MODEL ONE-GENERATOR INFINITE-BUS SYSTEM

$$\text{Swing equation: } \delta = \frac{\pi f_0}{H} \iint (P_m - \frac{V_1 V_2 \sin \delta}{X_{d1} + X_{d2} + X_L}) dt dt$$



H : inertia constant of the generator, f_0 : nominal frequency, δ : angle between V_1 and V_2 (V_1 is voltage reference, $V_1 = 1.0 \angle 0^\circ$), P_m : generator mechanical power, X_{di} : generator direct axis reactance



The OTA after Gilbert sine() converts V to I , and $A\beta$ is the overall gain of both circuits

Steady state equivalence:

$$V_2 = V_{o2} + \int \frac{g_m}{C_2} \int \frac{I_m - I_e(V_2)}{C_1} dt dt$$

$$V_2 = \frac{g_m}{C_1 C_2} \iint (I_m - A\beta \sin(V_2)) dt dt$$

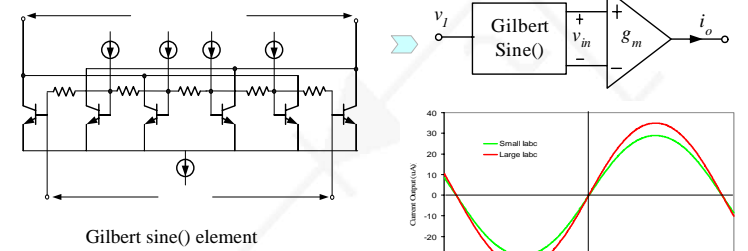
$$P_m = \frac{V_1 V_2 \sin \delta}{X_{d1} + X_{d2} + X_L}$$

$$I_m = A\beta \sin(V_2)$$

The overall accuracy of the emulation, the solution to the generator angle delta, is dependent on a host of factors including the respective accuracies of components. Here, sine shaper and double integrator are provided with the purpose of identifying qualifying and quantifying certain inaccuracies

OTA APPLICATIONS IN POWER SYSTEM EMULATOR

OTA-based Sine Shaper:

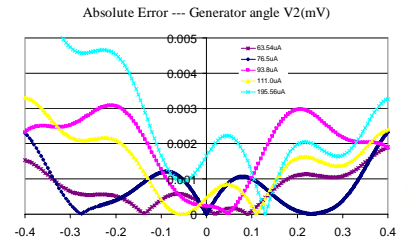
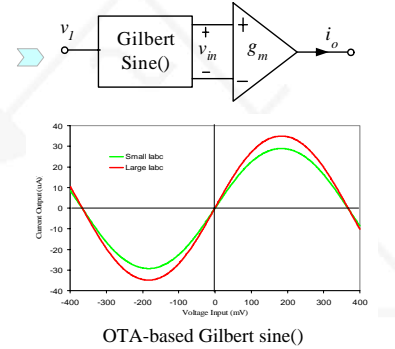


One of the identifiable factors affecting the accuracy of the generator angle is the accuracy of the sine shaper.

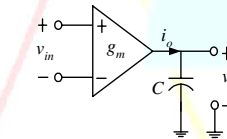
Vary I_{abc} value of the OTA to minimize the offset voltage, increase accuracy

Compare with ideal sine wave, quantify error in case of different I_{abc}

Optimal I_{abc} value exists so that the sine shaper outputs symmetrical wave form with minimum offset voltage.



OTA-based Integrator:



Single integrator: $v_{C1} = \frac{1}{C_1} \int_0^t i_0(x) dx + v_{C1}(0)$
 $v_{C1}(t) = \frac{h I_{abc}}{C_1} \int_0^t v_{in}(x) dx + v_{C1}(0)$

Double integrator: $v_0(t) = v_{C2}(t) = \frac{h^2 I_{abc}^2}{C_1 C_2} \int_0^t \int_0^t v_{in}(x) dx$

Double integrator decides the inertia constant of the generator.

Double integrator and hence I_{abc} determines the region of convergence to the eventual steady state solution (by appropriate initial condition sensitivity evaluation) in addition to emulation speed.

FUTURE WORKS

- Sensitivity evaluation of emulation speed to delay characteristics of individual emulator component circuits
- Error minimization for large scale power system
- Parameter optimization of the OTA applications in large scale power system

ACKNOWLEDGEMENTS

The authors would like to thank the Department of Energy for their financial support under Grant No. CH11171.